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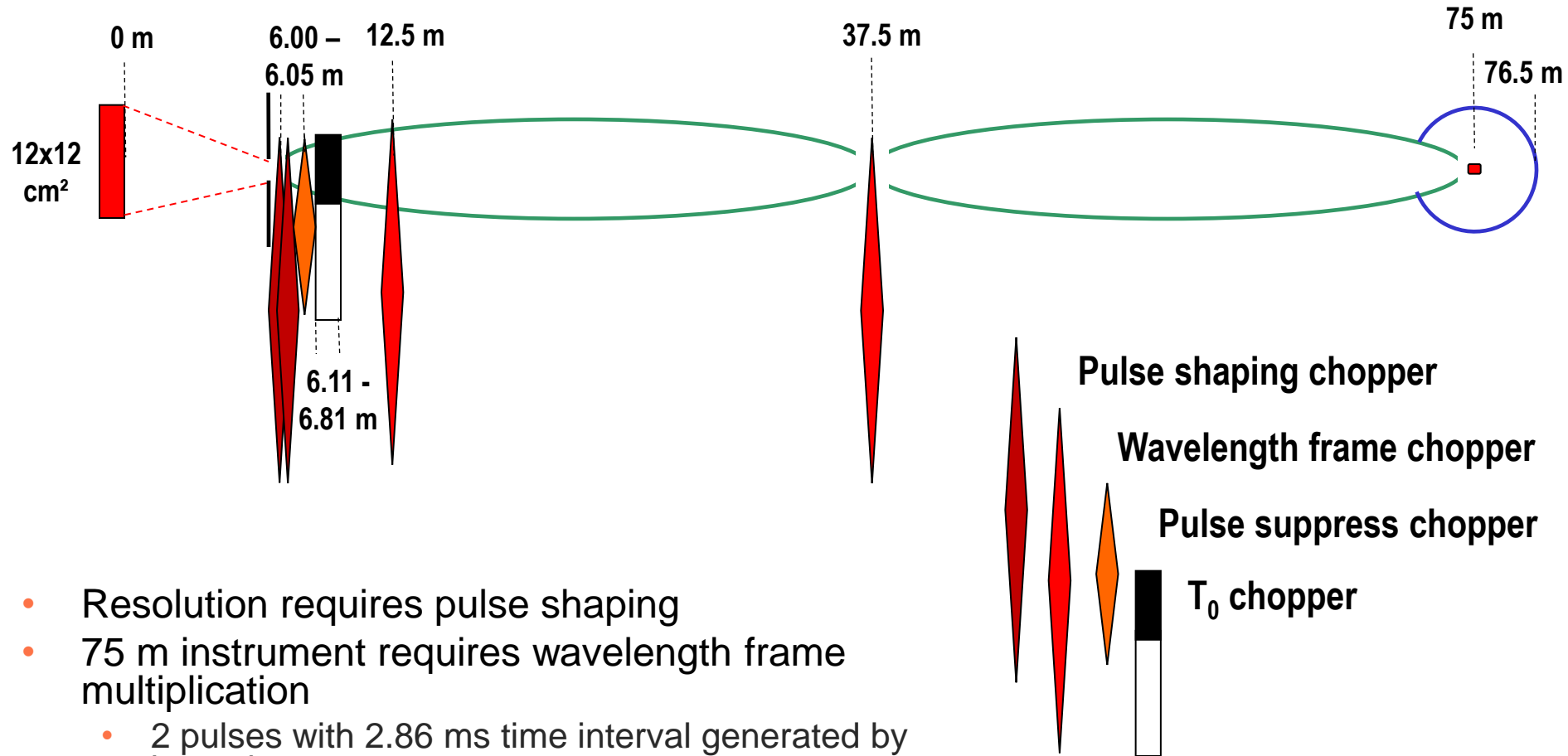
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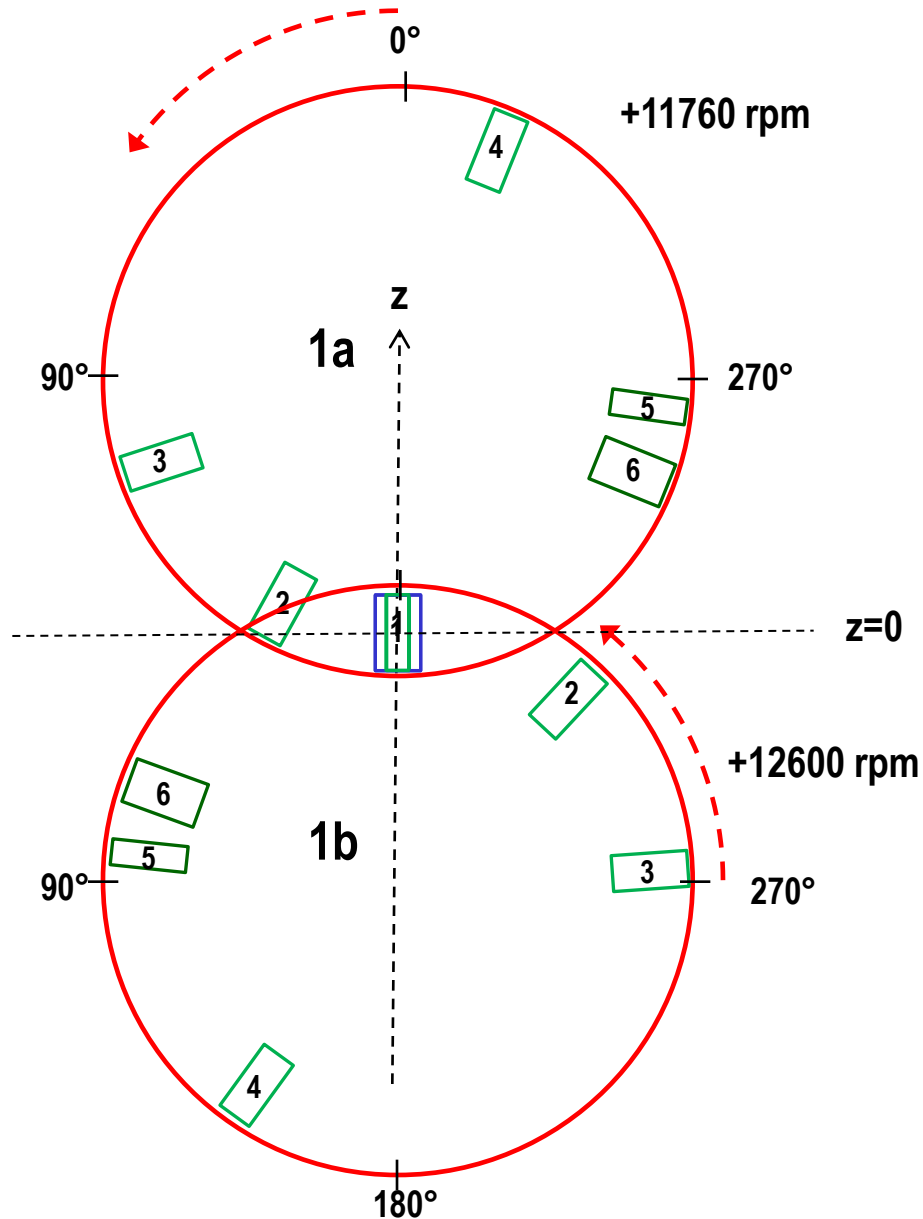
Simulations of the ESS Diffractometer PowHow

**K. Lieutenant
W. Schweika
N. Violini**





- Resolution requires pulse shaping
- 75 m instrument requires wavelength frame multiplication
 - 2 pulses with 2.86 ms time interval generated by beat chopper system
 - Suppression chopper removes unwanted neutrons e.g. from tail
- T₀ chopper for background reduction



Short pulses - High resolution

Windows 1 + 4: $14 \times 14 \times 60 = 11760$ rpm
 $15 \times 14 \times 60 = 12600$ rpm

Windows 1 + 3: $5 \times 14 \times 60 = 4200$ rpm
 $6 \times 14 \times 60 = 5040$ rpm

Windows 1 + 2: $2 \times 14 \times 60 = 1680$ rpm
 $3 \times 14 \times 60 = 2520$ rpm

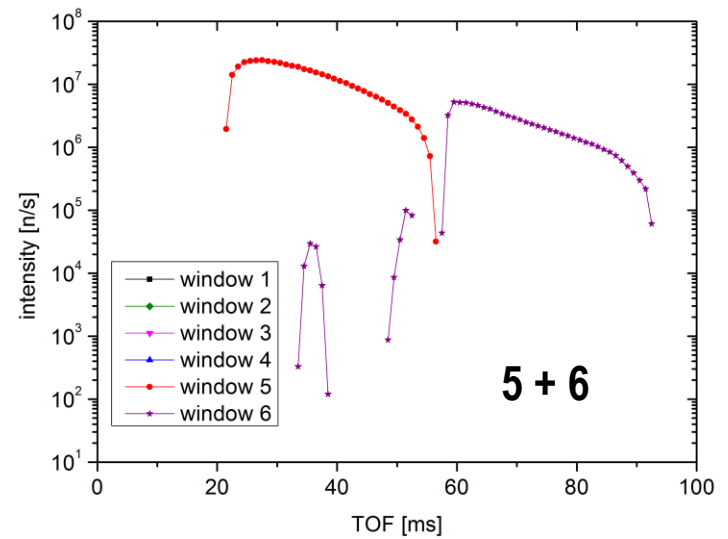
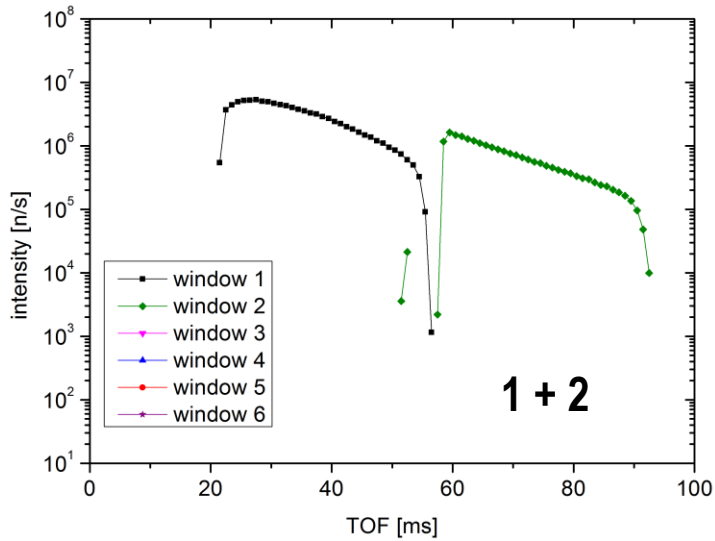
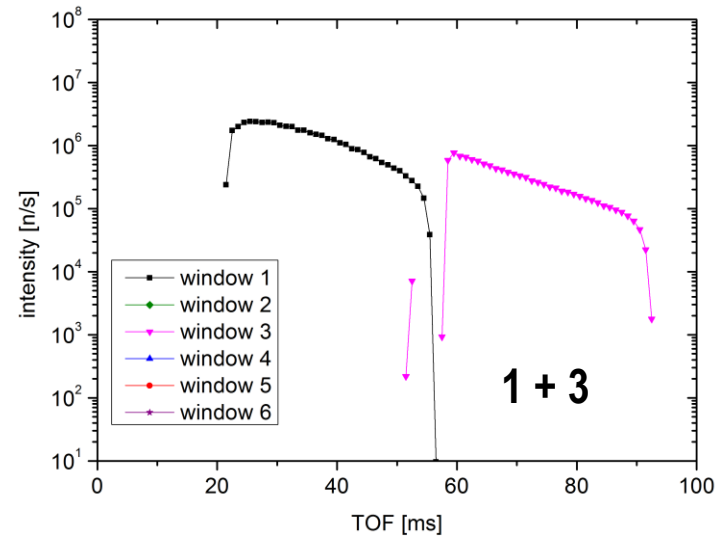
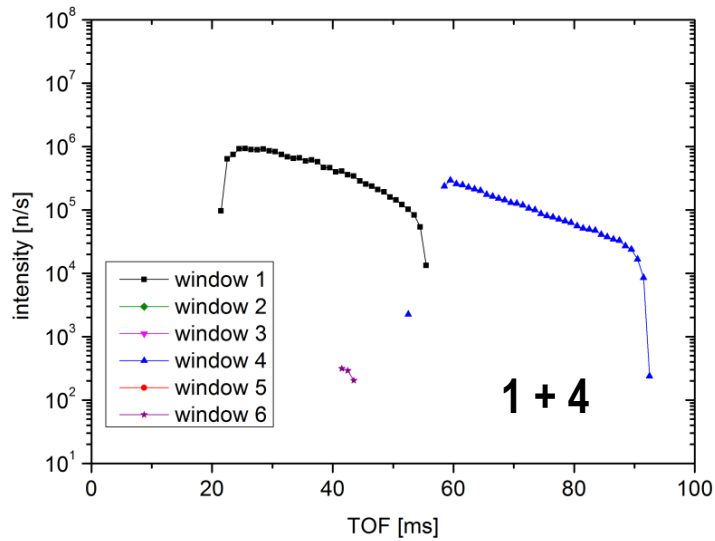
Windows 5 + 6: $1 \times 14 \times 60 = 840$ rpm
 $1 \times 14 \times 60 = 840$ rpm

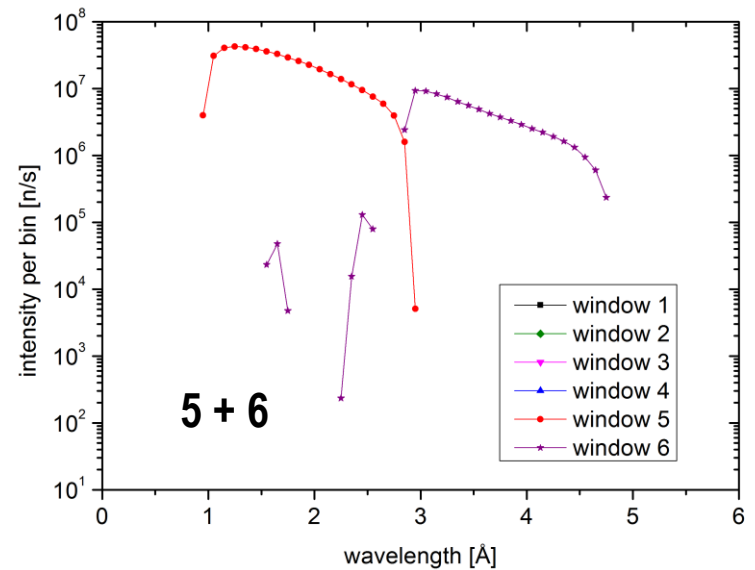
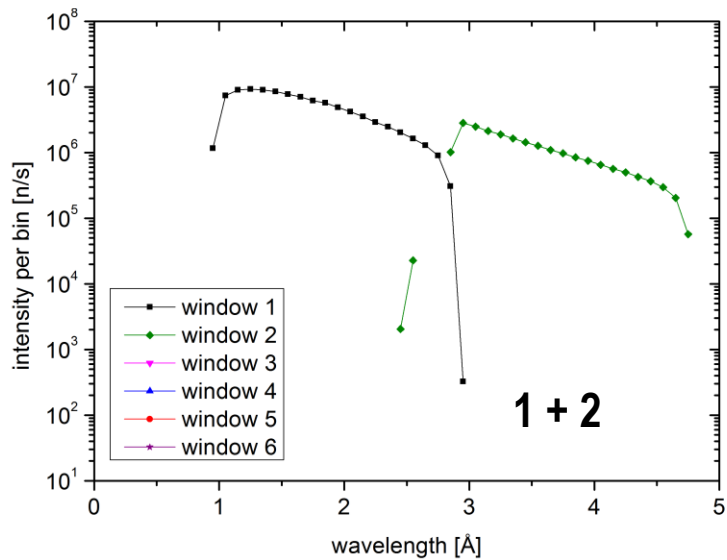
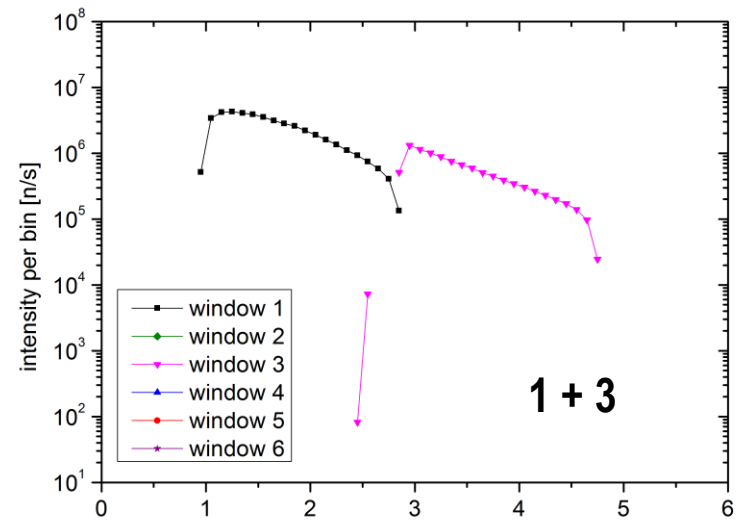
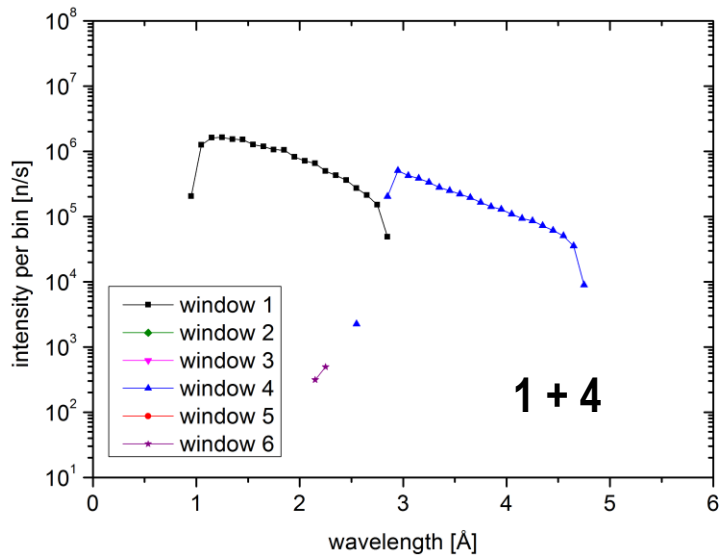
Long pulses - Low resolution

Chopper Data

L [m]	Delλ [Å]	λ ₁ [Å]	λ ₂ [Å]	λ _{ave} [Å]
75.0	3.768	1.943	3.827	2.885

chop	Component description	N	Chopper Parameters											Windows			TOF and Phase										
			position [m]	speed [rpm]	radius [mm]	DelH [cm]	H _{beam} [cm]	H _{wnd} [mm]	Posaxial [cm]	absorp.	zero time	neutr. pass	set color	no	pos [deg]	width [deg]	shape	T [ms]	tof [ms]	and t ₀ [ms]	Phase t _{ges} [ms]	t _{min} [ms]	t _{max} [ms]	φ _{run} [deg]	φ _{0,red} [deg]		
1a	pulse shaping	14	6.000	11760	37.5	0.5	4.0	5.0	35.0	ideal	no	yes	no	1	180.00	1.637	rectang.	5.102	2.947	1.429	4.375				308.73	-308.73	
		2	6.000	1680										2	151.20	3.274	rectang.	35.714	5.804	1.429	7.233				72.90		
	above	5	6.000	4200										3	108.00	3.274	rectang.	14.286	5.804	1.429	7.233				182.26		
		14	6.000	11760										4	338.40	3.274	rectang.	5.102	5.804	1.429	7.233				510.33		
		1	6.000	840										5	262.08	2.456	rectang.	71.429	2.947	1.429	4.375				22.05	-104.13	
		1	6.000	840										6	247.68	4.911	rectang.	71.429	5.804	1.429	7.233				36.45		
1b	pulse shaping	15	6.012	12600	37.5	0.5	4.0	5.0	-35.0	ideal	no	yes	yes	1	0.00	1.637	rectang.	4.762	2.953	1.429	4.381				331.22	-331.22	
		3	6.012	2520										2	316.80	3.274	rectang.	23.810	5.816	1.429	7.244				109.53		
		6	6.012	5040										3	273.60	3.274	rectang.	11.905	5.816	1.429	7.244				219.06		
	below	15	6.012	12600										4	144.00	3.274	rectang.	4.762	5.816	1.429	7.244				547.66		
		1	6.012	840										5	83.95	2.456	rectang.	71.429	2.953	1.429	4.381				22.08	-106.03	
		1	6.012	840										6	69.55	4.911	rectang.	71.429	5.816	1.429	7.244				36.51		
2	pulse suppr. below		6.050	840	15.0	0.5	4.0	5.0	-12.5	ideal	no	yes	no		0.00	18.800	radial	71.429	4.412	1.429	5.840	3.975	7.706	29.44	-29.44		
3a	T0 below		6.110	1680	15.0	0.5	4.0	5.0	-12.5	ideal	no	yes	no	1	90.00	144.0	radial	35.714	0.000	1.429	1.429				14.40	-14.40	
														2	270.00	144.0	radial										
3b	T0 below		6.460	1680	15.0	0.5	4.0	5.0	-12.5	ideal	no	yes	no	1	90.00	144.0	radial										-14.40
														2	270.00	144.0	radial										
3c	T0 below		6.810	1680	15.0	0.5	4.0	5.0	-12.5	ideal	no	yes	no	1	90.00	144.0	radial										-14.40
														2	270.00	144.0	radial										
4	FO below		12.500	10080	37.5	2.0	12.0	14.5	-29.5	ideal	no	yes	no		0.00	240.0	radial	5.952	6.139	1.429	7.568				457.70	-97.70	
5	FO below		37.500	3360	37.5	2.0	4.0	6.5	-33.5	ideal	no	yes	no		0.00	310.0	radial	17.857	18.418	1.429	19.846				400.10	-40.10	

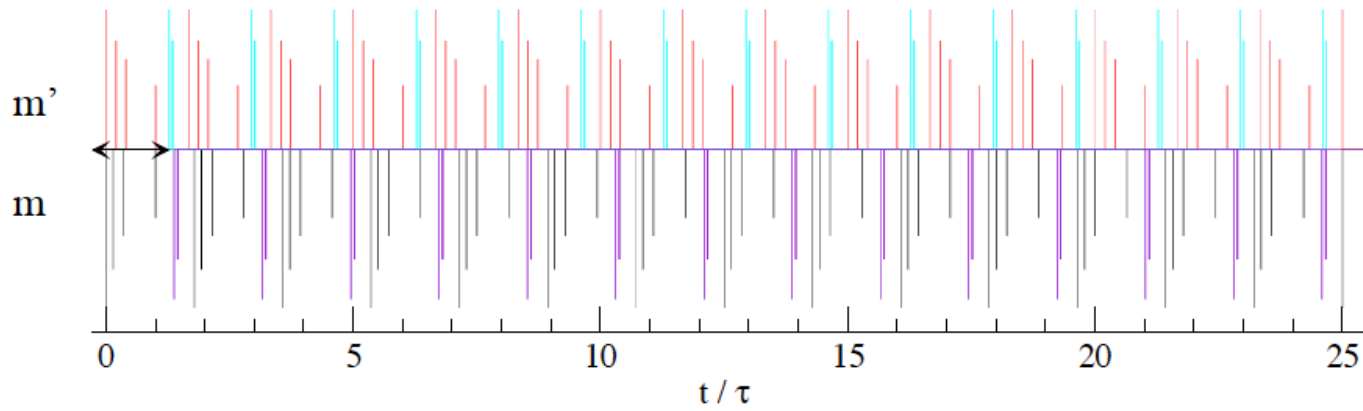




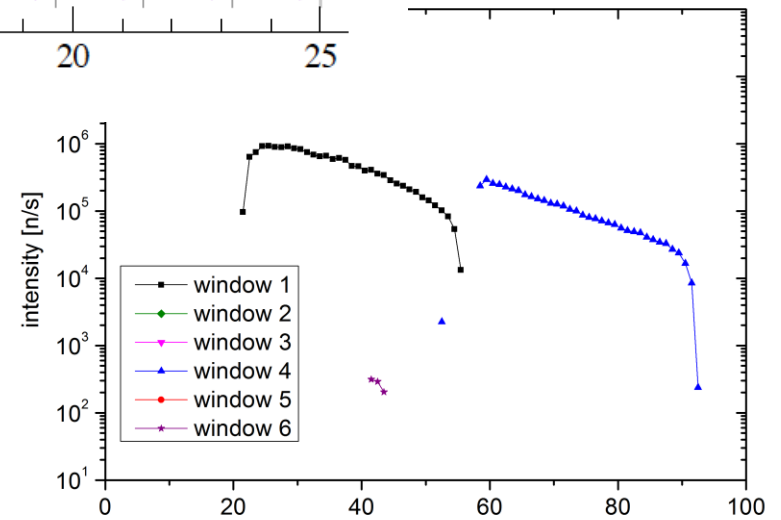
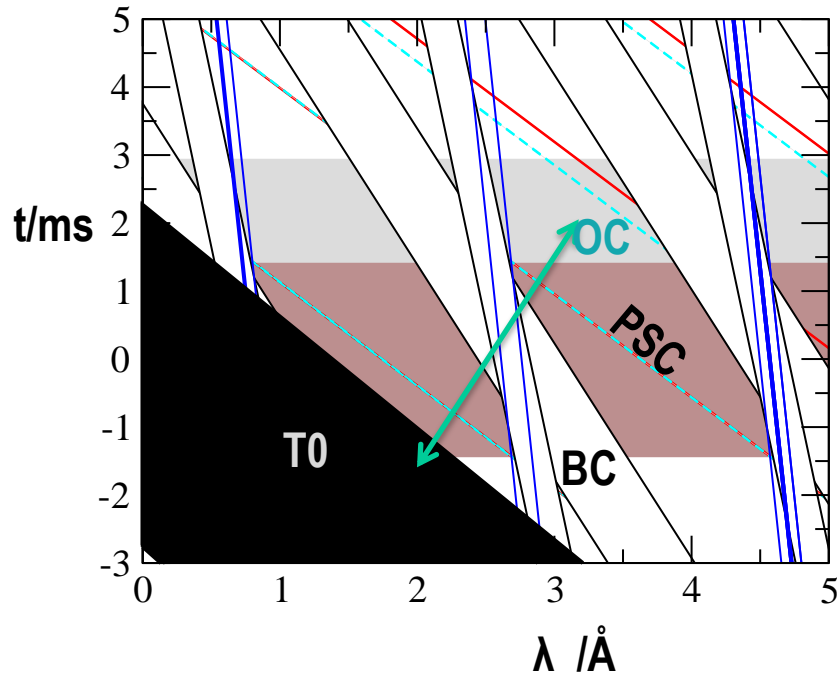
- TOF spectra well separated at the detector
- Wavelength spectra overlap
- The spectra have undesired contaminations $<10^{-3}$
 - needs analysis and improvements if possible



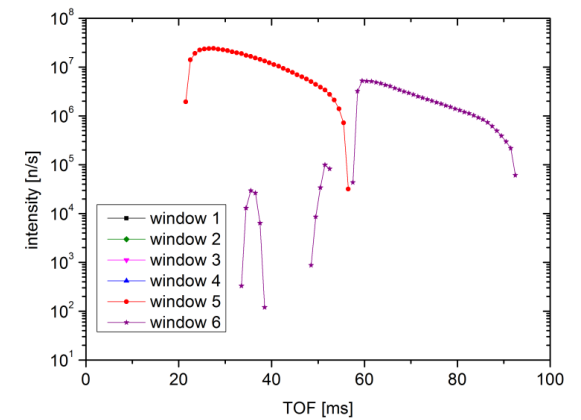
Chopper System: Contaminations



acceptance diagram



ESS pulse

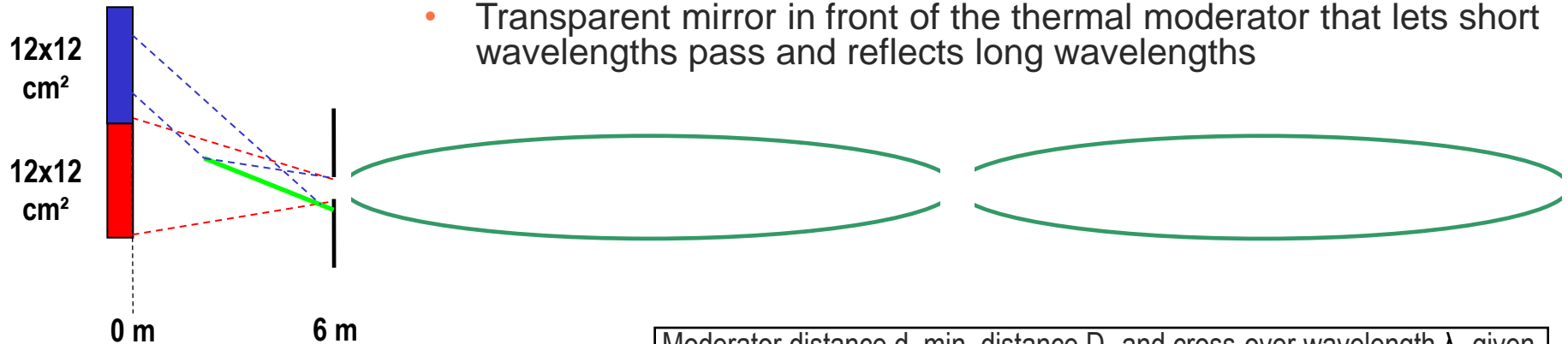




- How to use both moderators ?

- Basic Idea

- Transparent mirror in front of the thermal moderator that lets short wavelengths pass and reflects long wavelengths



Moderator distance d , min. distance D_0 and cross-over wavelength λ_c given
- choose mirror coating m
→ mirror inclination: $\alpha = 0.1 m \lambda_c$
→ mirror center: $D_{\text{mirr}} = d/\tan(2\alpha)$
→ sym. mirror length: $L_{\text{mirr}} = 2(D_{\text{mirr}} - D_0)/\cos(\alpha)$

- Only 1 free parameter

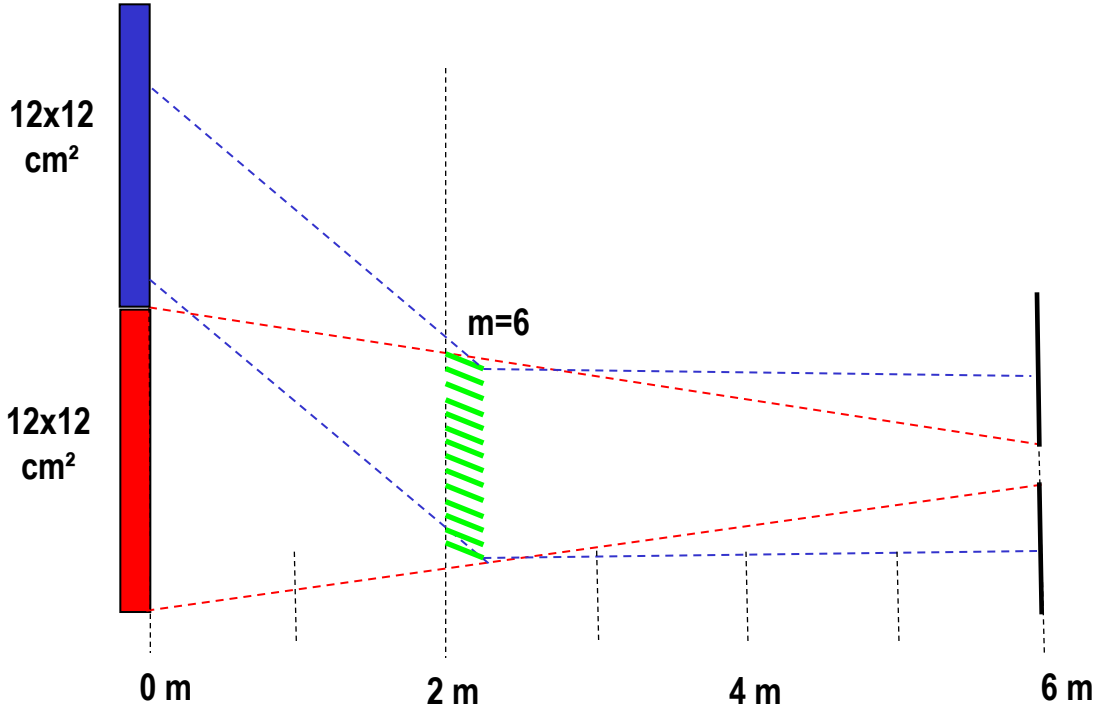
- Mirror coating and cross-over wavelength determines inclination angle (e.g. 1.175° for $m=5$ and 2.35 Ang cross-over wavelength)
- => distance between moderator centers determines center position
- => minimal distance fixes mirror size

- Drawbacks

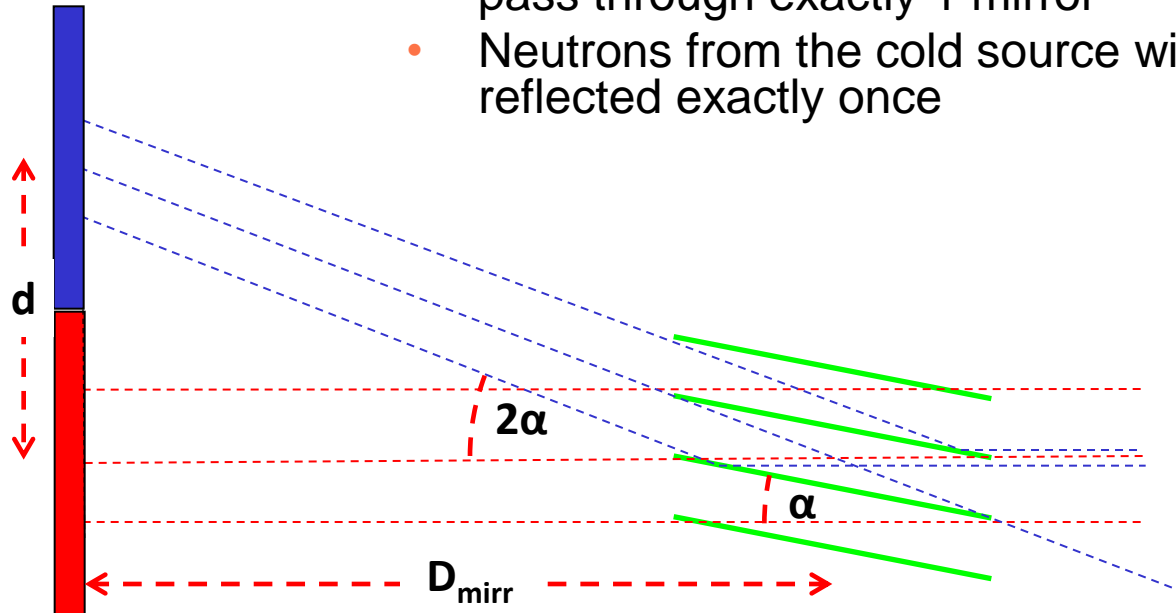
- Difficult installation and exchange



Usual Approach: As close as Possible to the Sample



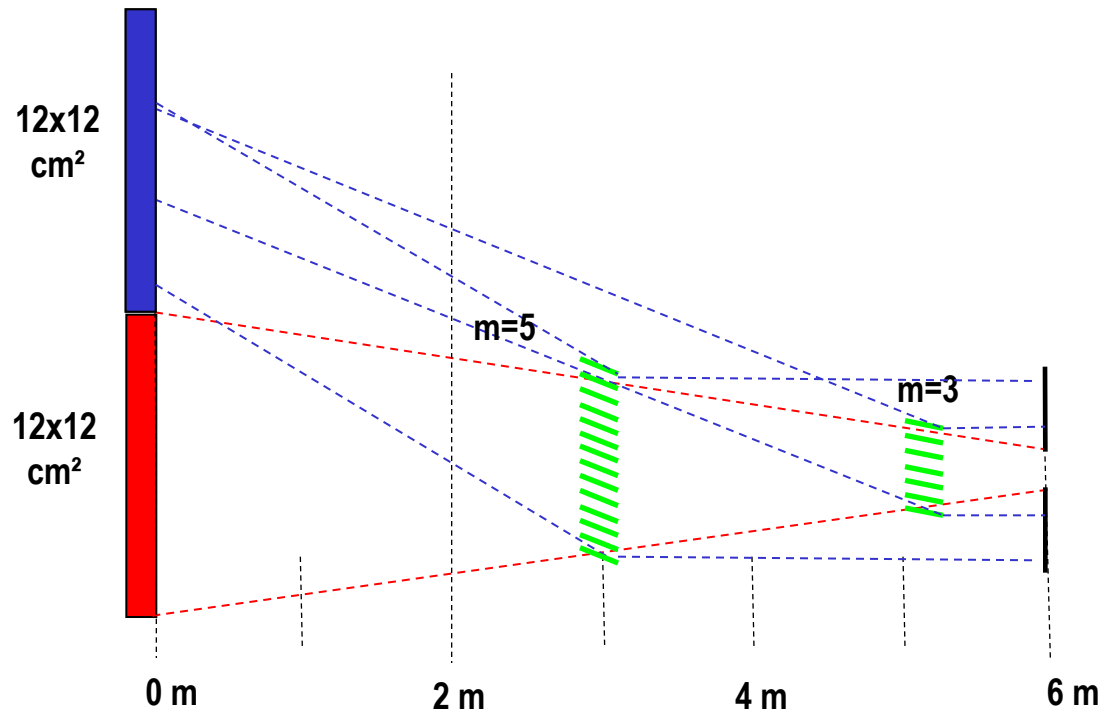
- Neutrons from the thermal source without divergence pass through exactly 1 mirror
- Neutrons from the cold source with divergence 2α are reflected exactly once



As for 1 mirror: $D_{\text{mirr}} = d / \tan(2 \cdot 0.1 \text{ m } \lambda_c)$
 Ideal distances for $d=0.12 \text{ m}$, $\lambda_c=2.35 \text{ \AA}$:

m	D_{mirr} [m]
7	2.110
6	2.462
5	2.955
4	3.695
3	4.928
2	7.392

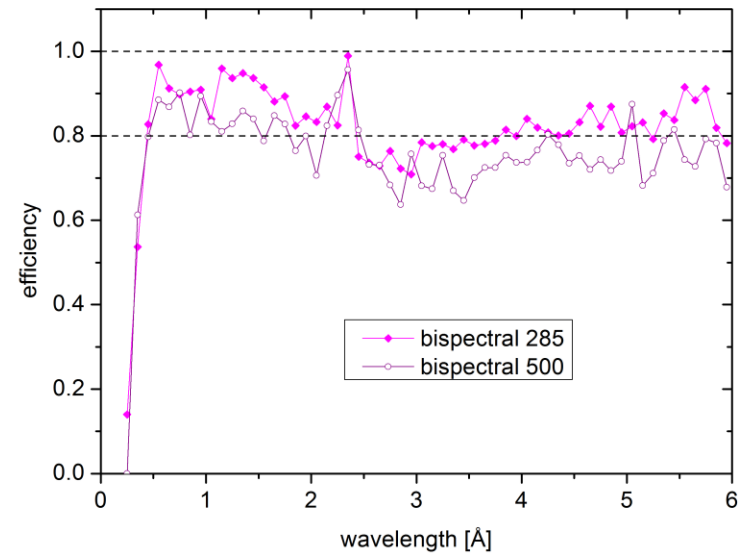
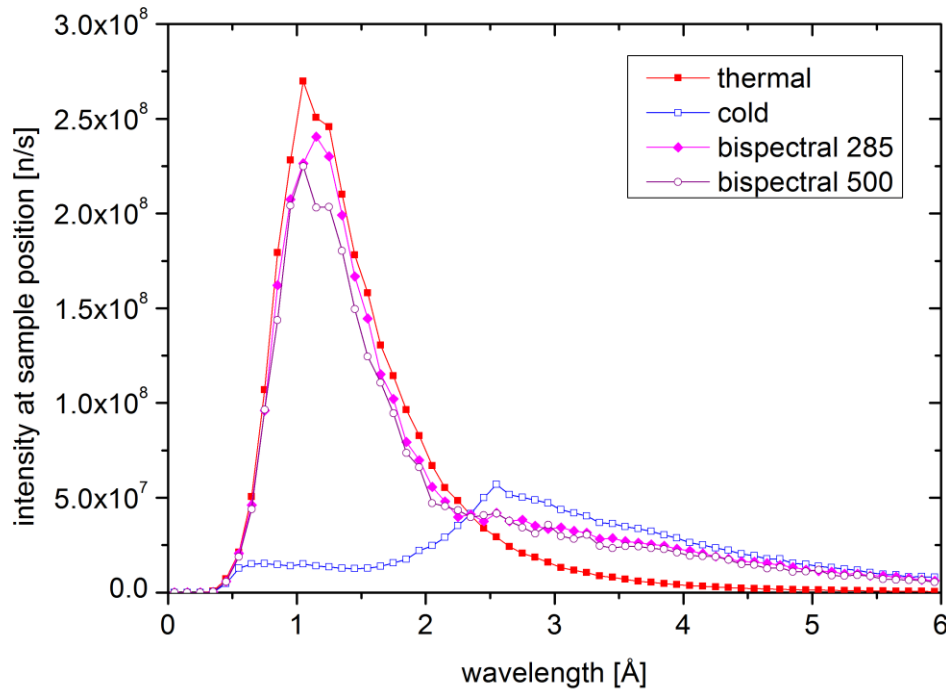
Chosen:
 2.975 m, $m=5$
 5.125 m, $m=3$



- **Advantages**

- Lower coating can be used
- Extraction system can be protected from radiation by shutter
- Easier access

- **But how is the Performance ?**



- **Result**
 - Efficiency is higher, if mirror is closer to moderator
- **Reasons**
 - Higher probability of reflection for divergent thermal neutrons
 - Higher probability of transmission for divergent cold neutrons
 - Longer paths through mirror

Thank you for your attention

**We like to thank the BMBF for their support through the contribution to the ESS update phase.
Work package K7: Simulationscode-Entwicklung, Helpdesk work package**